## Vapor-Phase Beckmann Rearrangement over Silica-Supported Boria Catalyst Prepared by Vapor Decomposition Method

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Received February 25, 1986; revised June 10, 1986

The present work introduced a new method of catalyst preparation which involved the vapor decomposition of  $B(OEt)_3$  onto silica gel to produce a silica-supported boria  $(B_2O_3/SiO_2)$ . A  $B_2O_3/SiO_2$  catalyst prepared by this method  $(B_2O_3 \text{ content } 34 \text{ wt}\%)$  showed high catalytic efficiency for the vapor-phase Beckmann rearrangement of cyclohexanone oxime (oxime conversion: 98%,  $\varepsilon$ -caprolactam selectivity: 96 mol%, at 250°C). The vapor decomposition  $B_2O_3/SiO_2$  was more active and selective at any  $B_2O_3$  content than the  $B_2O_3/SiO_2$  obtained by the ordinary impregnation method using  $H_3BO_3$ . The amounts of the acid sites whose acid strengths exceeded 80 kJ/mol in terms of the differential heat of adsorption of ammonia (DHA) were 0.7 and 0.4 mmol/g for the most active vapor decomposition  $B_2O_3/SiO_2$  and the most active impregnation  $B_2O_3/SiO_2$ , respectively. The vapor decomposition of facted uniform deposition of  $B_2O_3$  on  $SiO_2$ , and produced a solid acid with relatively uniform distribution of acid strength. It is suggested that the acid strength ( $H_0$ ) of an effective catalyst pertinent to the vapor-phase Beckmann rearrangement should be less than -5.6 which approximately corresponds to a DHA value of more than 80 kJ/mol. © 1986 Academic Press, Inc.

#### I. INTRODUCTION

The vapor decomposition of metal alkoxides or halides onto several inorganic materials has recently been applied to catalyst preparation as well as to modification of catalytic property of zeolites. Murakami et al. have reported that the size of the entry pore of mordenite can be narrowed by depositing SiO<sub>2</sub> by means of vapor decomposition using Si(OCH<sub>3</sub>)<sub>4</sub> or SiCl<sub>4</sub>. This modified mordenite showed higher selectivity of light hydrocarbons  $(C_1-C_3)$  when applied as a methanol conversion catalyst (1, 2). The authors have recently attempted to prepare several solid acids by means of vapor decomposition, expecting that such a method of catalyst preparation may produce more active and selective solid acids with high uniformity in acid property. In fact, according to our preliminary studies (3, 4), the supported boria catalysts prepared through the vapor decomposition of a boron ester onto silica gel and  $\gamma$ -alumina (B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub>) and  $B_2O_3/Al_2O_3$ ) showed higher activities for the vapor-phase Beckmann rearrangement of cyclohexanone oxime, compared with those obtained through the conventional impregnation method using boric acid.

In the present study, the silica-supported boria catalysts prepared by the vapor decomposition method using B(OEt)<sub>3</sub> will be characterized in detail with respect to the acid property and the catalytic efficiency for the vapor-phase Beckmann rearrangement of cyclohexanone oxime, in comparison with the boria catalysts obtained by the ordinary impregnation method. The reason for selecting the Beckmann rearrangement as a test reaction is that supported boria catalysts such as boria-alumina (5-8) have long been known as favorable catalysts for this reaction but there is still plenty of room for improvement, particularly in the selectivity to  $\varepsilon$ -caprolactam as well as in catalyst life in view of practical application.



FIG. 1. An apparatus for the catalyst preparation through vapor decomposition.

#### **II. EXPERIMENTAL**

## Catalyst

1. Vapor decomposition  $B_2O_3/SiO_2$ . An apparatus for the catalyst preparation through vapor decomposition technique is shown in Fig. 1. A specific silica support having a surface area of 281  $m^2/g$  and a pore volume of 1.35 ml/g (Fuji Davison Chemical, ID type) was employed in all experiments, except for a case of the examination on the effects of physical property of silica support. Silica gel (0.5-1.0 g, 24-60 mesh granules) was placed in a Pyrex glass reactor, and B(OEt)<sub>3</sub> vapor was brought into contact with SiO<sub>2</sub> at 250-400°C for 0.1-6.0 h in a stream of air. The flow rates of B(OEt)<sub>3</sub> and air were 3.5 mmol/h and 115 ml/min, respectively. There was observed no carbon left on the resulting catalysts. The B<sub>2</sub>O<sub>3</sub> content of catalyst was determined from the weight increase of SiO<sub>2</sub> after the vapor decomposition treatment; the data obtained by this method agreed closely with those by the alkalimetric titration of the H<sub>3</sub>BO<sub>3</sub> extracted from catalyst with hot water.

2. Impregnation  $B_2O_3/SiO_2$ . The impregnation catalyst was prepared by impregnating the same silica support with aqueous H<sub>3</sub>BO<sub>3</sub> followed by calcination at 350°C for 3 h.

### Beckmann Rearrangement

The vapor-phase Beckmann rearrangement of cyclohexanone oxime was carried out using a fixed-bed continuous flow apparatus under atmospheric pressure. The reaction temperature, which was measured by a thermocouple placed in the catalyst bed, was maintained at 250°C. A mixture of the oxime, benzene as a diluent, and N<sub>2</sub> was passed in a mole ratio of 1:13:16 through the catalyst bed (0.2 g) packed in a 15-mmi.d. Pyrex glass reactor at a WHSV of 0.81 h<sup>-1</sup> in terms of the oxime. The reactor effluent was collected in a trap and analyzed by GLC using a PEG 20M column (1 m). The major by-products included cyclohexanone and hex-5-enenitrile.

#### Analysis

The desorption spectra of pyridine on  $B_2O_3/SiO_2$  catalysts were measured by use of a conventional TPD apparatus. A catalyst sample (30 mg) was preheated in a TPD cell at 400°C for 1 h in a stream of He (115 ml/min). Pyridine (10  $\mu$ l) was injected at 300°C, and the cell was cooled rapidly to 25°C. The TPD measurement was started from 25°C at a heating rate of 10°C/min.

The differential heat of adsorption of ammonia was measured by use of a multipurpose calorimeter (Tokyo RIKO, Model MPC-11). The sample was preheated at 400°C for 1 h.

The scanning electron microscopy for the examination of catalyst surface was performed using a JEOL JSM-T20 instrument.

## III. RESULTS

Figure 2 shows the change in catalytic activity for the Beckmann rearrangement with the time on stream at 300 and 250°C. When the reaction was performed at 300°C, the catalytic activity of impregnation  $B_2O_3/$ SiO<sub>2</sub> gradually decreased with the time on stream owing to coking, but little change in activity was observed with vapor decomposition  $B_2O_3/SiO_2$  up to 5 h of the run. In the present study, however, the reaction data were taken at 250°C in order to compare the catalytic efficiency of vapor decomposition  $B_2O_3/SiO_2$  with that of impregnation  $B_2O_3/$  $SiO_2$ , because the oxime conversion at 300°C were too high to discuss the difference in catalytic efficiency between those two



FIG. 2. The change in catalytic activity of  $B_2O_3/SiO_2$ with the time on stream. (1) Vapor decomposition  $B_2O_3/SiO_2$  ( $B_2O_3$ , 32 wt%), (2) impregnation  $B_2O_3/SiO_2$ ( $B_2O_3$ , 26 wt%), reaction temperature 300°C, (3) vapor decomposition  $B_2O_3/SiO_2$  ( $B_2O_3$ , 25 wt%), (4) impregnation  $B_2O_3/SiO_2$  ( $B_2O_3$ , 19 wt%), reaction temperature 250°C.

catalysts in detail. At 250°C, however, the oxime conversion decreased more rapidly with the time on stream than at 300°C owing to faster coke formation which was caused probably by slower desorption of high boiling point products. Hence, the average oxime conversion and lactam selectivity obtained between 3 and 4 h after the reactant feed were taken as the standard data; mass balance was not completed during initial 3 h of each run at this reaction temperature.

## Effects of Vapor Decomposition Conditions

Figure 3 shows the influence of vapor decomposition temperature on the catalytic activity of the resulting  $B_2O_3/SiO_2$ . The rate of  $B_2O_3$  deposition on  $SiO_2$  surface was greatly influenced by vapor decomposition temperature. The  $B_2O_3$  content increased with increasing temperature, and the maximum  $B_2O_3$  content was attained at 350°C. The oxime conversion was correlated well to the  $B_2O_3$  content, but the lactam selectivity decreased markedly at above 350°C.

Figure 4 gives the influence of the duration of  $B(OEt)_3$  feed at a constant rate. The  $B_2O_3$  content increased monotonously until 3 h of  $B(OEt)_3$  feed and then leveled off. The oxime conversion depended on the



FIG. 3. The effect of vapor decomposition temperature. (1) Oxime conversion, (2) lactam selectivity; vapor decomposition condition,  $B(OEt)_3$  feed 3.5 mmol/ h for 3 h; reaction condition, 250°C.

B<sub>2</sub>O<sub>3</sub> content, but when the duration of B(OEt)<sub>3</sub> feed exceeded 3 h, the lactam selectivity decreased rapidly. Thus the B<sub>2</sub>O<sub>3</sub> content could be adjusted by changing either vapor decomposition temperature or the duration of B(OEt)<sub>3</sub> feed. The best B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> catalyst containing 34 wt% of B<sub>2</sub>O<sub>3</sub> was obtained under the condition of 350°C for 3 h at a B(OEt)<sub>3</sub> feed rate of 3.5 mmol/h. This catalyst showed an oxime conversion of 98% with a lactam selectivity of 96% at a reaction temperature of 250°C.

Figure 5 illustrates the change in catalytic performance with  $B_2O_3$  content, comparing vapor decomposition  $B_2O_3/SiO_2$  with im-



FIG. 4. The effect of the duration of  $B(OEt)_3$  feed. (1) Oxime conversion, (2) lactam selectivity; vapor decomposition condition, 350°C,  $B(OEt)_3$  feed 3.5 mmol/ h for 3 h; reaction condition, 250°C.



FIG. 5. The effect of  $B_2O_3$  content. (1) Oxime conversion of impregnation  $B_2O_3/SiO_2$ , (2) oxime conversion of vapor decomposition  $B_2O_3/SiO_2$ , (3) lactam selectivity of impregnation  $B_2O_3/SiO_2$ , (4) lactam selectivity of vapor decomposition  $B_2O_3/SiO_2$ ; reaction condition, 250°C.

pregnation  $B_2O_3/SiO_2$ . Both the oxime conversion and the lactam selectivity increased with the  $B_2O_3$  content, but the oxime conversion over impregnation  $B_2O_3/SiO_2$  began to decrease at a  $B_2O_3$  content above 20 wt%. It is obvious that vapor decomposition  $B_2O_3/SiO_2$  excelled impregnation  $B_2O_3/SiO_2$  in the catalytic efficiency for the Beckmann rearrangement.

When N<sub>2</sub> was employed as a carrier gas in place of air in the vapor decomposition operation, only a little deposition of  $B_2O_3$ (0.8 wt%) was attained under the condition of 350°C for 3 h at a B(OEt)<sub>3</sub> feed rate of 3.5 mmol/h. The resulting  $B_2O_3/SiO_2$  was as inactive as SiO<sub>2</sub> support itself for the Beckmann rearrangement. On the other hand, when steam was used in place of air in the vapor decomposition operation, a  $B_2O_3/$ SiO<sub>2</sub> having a B<sub>2</sub>O<sub>3</sub> content of 29 wt% was obtained. But in this case B<sub>2</sub>O<sub>3</sub> was deposited exclusively on the upper side of the  $SiO_2$  bed packed in the reactor for vapor decomposition, because B(OEt)<sub>3</sub> had already changed into B<sub>2</sub>O<sub>3</sub> or H<sub>3</sub>BO<sub>3</sub> through hydrolysis in the gas phase before the borate reached the surface of SiO<sub>2</sub> particles. The B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> prepared by the vapor decomposition using H<sub>2</sub>O showed lower catalytic activity (oxime conversion; 82%; lactam selectivity, 93 mol%, at 250°C) than the  $B_2O_3/SiO_2$  prepared by use of air. It is, therefore, necessary for uniform  $B_2O_3$  deposition to decompose B(OEt)<sub>3</sub> with O<sub>2</sub> not with H<sub>2</sub>O.

## Effects of Physical Property of SiO<sub>2</sub> Support

Table 1 summarizes the influences of physical property of SiO<sub>2</sub> support on the efficiency of vapor decomposition catalyst. The amount of the  $B_2O_3$  deposited on SiO<sub>2</sub> depended neither on the surface area nor on the average pore diameter, but depended on the pore volume. The larger the pore volume of support was, the more  $B_2O_3$  could be deposited to give more active catalysts.

Table 2 represents the effect of pretreatment of SiO<sub>2</sub> support on the catalytic activity of the resulting  $B_2O_3/SiO_2$ . When the calcination temperature was below 600°C, no appreciable influences were observed both on the  $B_2O_3$  content and on the catalytic activity. However, when SiO<sub>2</sub> support was treated at 800°C, the catalyst obtained became less active because of the decrease in surface area, although its  $B_2O_3$  content was as much as 30 wt%. Probably, when

TABLE 1

The Effect of Physical Property of SiO<sub>2</sub> Support

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Physical property			Vapor decomposition B <sub>2</sub> O <sub>3</sub> /SiO <sub>2</sub>			
281 192 1.35 34 98.6 96.4   70 583 1.02 32 66.3 94.0   585 51 0.86 15 69.6 91.0   115 223 0.64 29 47.1 95.0   347 93 0.81 41 37.7 97.1   649 36 0.59 7.2 22.3 58.5   166 140 0.58 2.0 11.1 35.6	SA (m <sup>2</sup> /g)	PD (A)	PV (ml/g)	B <sub>2</sub> O <sub>3</sub> <sup>b</sup> content (wt%)	Oxime <sup>c</sup> conversion (%)	Lactam selectivity (mol%)	
70 583 1.02 32 66.3 94.0   585 51 0.86 15 69.6 91.0   115 223 0.64 29 47.1 95.0   347 93 0.81 41 37.7 97.1   649 36 0.59 7.2 22.3 58.5   166 140 0.58 2.0 11.1 35.6	281	192	1.35	34	98.6	96.4	
585 51 0.86 15 69.6 91.0   115 223 0.64 29 47.1 95.0   347 93 0.81 41 37.7 97.1   649 36 0.59 7.2 22.3 58.5   166 140 0.58 2.0 11.1 35.6	70	583	1.02	32	66.3	94.0	
115 223 0.64 29 47.1 95.0   347 93 0.81 41 37.7 97.1   649 36 0.59 7.2 22.3 58.5   166 140 0.58 2.0 11.1 35.6	585	51	0.86	15	69.6	91.0	
347 93 0.81 41 37.7 97.1   649 36 0.59 7.2 22.3 58.5   166 140 0.58 2.0 11.1 35.6	115	223	0.64	29	47.1	95.0	
649 36 0.59 7.2 22.3 58.5   166 140 0.58 2.0 11.1 35.6	347	93	0.81	41	37.7	97.1	
166 140 0.58 2.0 11.1 35.6	649	36	0.59	7.2	22.3	58.5	
	166	140	0.58	2.0	11.1	35.6	

 $^{a}$  SA, specific surface area; PD, average pore diameter; PV, pore volume. These values were given by the suppliers.

<sup>b</sup> Vapor decomposition, 350°C, 3 h; B(OEt)<sub>3</sub>, 3.7 mmol/h; air, 115 ml/ min.

<sup>c</sup> Average conversion of 3-4 h at 250°C.

TA	BL	Æ	2

The Effect of Calcination of SiO<sub>2</sub> Support

Calcination	Vapor decomposition B <sub>2</sub> O <sub>3</sub> /SiO <sub>2</sub> catalyst					
of SiO <sub>2</sub> <sup><i>a</i></sup> (°C)	B <sub>2</sub> O <sub>3</sub> <sup>c</sup> content (wt%)	BET surface area (m²/g)	Oxime conversion (%)	Lactam selectivity (mol%)		
350 <sup>b</sup>	34	135	98.6	96.4		
450	30		94.9	95.4		
600	28	_	95.8	97.0		
800	30	85.4	72.4	96.8		

<sup>a</sup> Calcination 3 h.

<sup>b</sup> Calcination 1 h.

<sup>c</sup> Vapor decomposition, 350°C, 3 h; B(OEt)<sub>3</sub>, 3.7 mmol/h; air, 115 ml/ min.

calcined at 800°C, the surface hydroxy groups of  $SiO_2$  were irreversibly dehydrated to reduce its surface area (9).

The pore size distribution of vapor decomposition  $B_2O_3/SiO_2$  was measured to study the process of  $B_2O_3$  deposition on the internal surface of  $SiO_2$  (Fig. 6).  $SiO_2$  support had a sharp peak at about 66 Å in addition to a broad peak at between 200 and 500 Å in the pore size distribution. When the  $B_2O_3$  content increased, the broad peak in a larger pore size region got smaller and the sharp peak at 66 Å shifted to a larger size of about 100 Å. At the same time, the pore volume was changed from 1.25 to 0.68 ml/ g. Similar tendency of the change in pore size distribution was observed with the impregnation  $B_2O_3/SiO_2$ .

# Characterization of Vapor Decomposition $B_2O_3/SiO_2$

Figure 7 shows the change in BET surface area of  $B_2O_3/SiO_2$  catalyst with  $B_2O_3$ content. The surface area decreased with increasing  $B_2O_3$  content with respect to both vapor decomposition and impregnation catalysts. The surface area of impregnation  $B_2O_3/SiO_2$  was larger than that of vapor decomposition  $B_2O_3/SiO_2$  at any  $B_2O_3$ content. This result implies that there remained more parts of the SiO<sub>2</sub> surface free from  $B_2O_3$  deposition in the case of impregnation catalyst.



FIG. 6. The pore size distribution of vapor decomposition  $B_2O_3/SiO_2$ . (1)  $SiO_2$  support, (2)  $B_2O_3/SiO_2$ ( $B_2O_3$ , 15 wt%), (3)  $B_2O_3SiO_2$  ( $B_2O_3$ , 34 wt%).

Figures 8a and b show the SEM images of the external surfaces of impregnation and vapor decomposition catalysts, respectively. Large B<sub>2</sub>O<sub>3</sub> crystallites (ca. 50  $\mu$ m) were deposited on the surface of impregnation catalyst. On the other hand, such large B<sub>2</sub>O<sub>3</sub> crystallites were hardly observed on the surface of vapor decomposition catalyst; the surface was as smooth as that of SiO<sub>2</sub> support itself.

Figure 9 illustrates the TPD profiles of



FIG. 7. The change in BET surface area. (1) Impregnation  $B_2O_3/SiO_2$ , (2) vapor decomposition  $B_2O_3/SiO_2$ . Dotted line denotes the surface area of  $SiO_2$  alone calculated from the amount of silica support in a unit weight of catalyst.





FIG. 8. The SEM images of  $B_2O_3/SiO_2$  external surfaces. (a) Impregnation  $B_2O_3/SiO_2$  ( $B_2O_3$ , 19 wt%), (b) vapor decomposition  $B_2O_3/SiO_2$  ( $B_2O_3$ , 34 wt%).



FIG. 9. The TPD profiles of the adsorbed pyridine on the vapor decomposition  $B_2O_3/SiO_2$ . (1)  $SiO_2$  support, (2)  $B_2O_3/SiO_2$  ( $B_2O_3$ , 10 wt%), (3)  $B_2O_3/SiO_2$  ( $B_2O_3$ , 22 wt%), (4)  $B_2O_3/SiO_2$  ( $B_2O_3$ , 33 wt%); all samples were treated at 400°C for 1 h prior to adsorption of pyridine.

the pyridine adsorbed on vapor decomposition B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> catalysts having different B<sub>2</sub>O<sub>3</sub> contents. The TPD profile of SiO<sub>2</sub> support showed only a single sharp peak at 100°C, and all the pyridine adsorbed was removed below 150°C. In contrast, the TPD profiles of B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> catalysts had the desorption maxima between 150 and 250°C. The amount of pyridine desorbed above 250°C increased with B<sub>2</sub>O<sub>3</sub> content. These results obviously tell that  $B_2O_3/SiO_2$  catalyst is more acidic than SiO<sub>2</sub> support, and that the amount of strongly acidic sites whose acid strengths correspond to pyridine desorption temperatures above 150°C increased with B<sub>2</sub>O<sub>3</sub> content.

The TPD profiles shown in Fig. 10 demonstrate the difference in acid property between vapor decomposition and impregnation  $B_2O_3/SiO_2$  whose  $B_2O_3$  contents are similar. Compared with the spectra of impregnation catalysts, each pyridine desorption peak on vapor decomposition catalyst slightly shifted to the higher temperature side.

Figure 11 shows the changes in the differential heat of adsorption of ammonia (DHA) on the most active vapor decomposition and impregnation catalysts, together with the data of  $SiO_2$  support. The level of DHA corresponds to the acid strength of  $B_2O_3/SiO_2$  and the adsorbed amount of ammonia means the number of acid sites. The initial value of DHA obtained with SiO<sub>2</sub> support was less than 80 kJ/mol, and the DHA decreased with increasing amount of adsorbed ammonia. The acid strength to catalyze the Beckmann rearrangement is thought to be at least 80 kJ/mol, because SiO<sub>2</sub> support alone had little activity for this reaction. The initial value of DHA on the impregnation catalyst was 110 kJ/mol, and the amount of adsorbed ammonia in the region where the DHA level exceeded 80 kJ/ mol was 0.4 mmol/g. As to vapor decomposition catalyst, the DHA change was similar to that of impregnation catalyst up to 0.2 mmol/g of adsorbed ammonia, but



FIG. 10. Comparative TPD profiles of vapor decomposition and impregnation  $B_2O_3/SiO_2$ . (1) Impregnation  $B_2O_3/SiO_2$  ( $B_2O_3$ , 8.0 wt%), (2) vapor decomposition  $B_2O_3/SiO_2$  ( $B_2O_3$ , 10 wt%), (3) impregnation  $B_2O_3/SiO_2$  ( $B_2O_3$ , 27 wt%), (4) vapor decomposition  $B_2O_3/SiO_2$  ( $B_2O_3$ , 22 wt%); (4) samples were treated at 400°C for 1 h prior to adsorption of pyridine.



FIG. 11. The change in the differential heat of adsorption of ammonia. (1) SiO<sub>2</sub> support, (2) impregnation  $B_2O_3/SiO_2$  ( $B_2O_3$ , 17 wt%), (3) vapor decomposition  $B_2O_3/SiO_2$  ( $B_2O_3$ , 34 wt%); all samples were treated at 400°C for 1 h prior to adsorption of ammonia.

the total amount of the effective acid sites having DHA values more than 80 kJ/mol was as much as 0.7 mmol/g. Moreover, it should be noted that the DHA curve observed with the vapor decomposition catalyst became flat in the range of adsorbed ammonia from 0.3 to 0.6 mmol/g.

#### **IV. DISCUSSION**

## Deposition of $B_2O_3$ on $SiO_2$ through Vapor Decomposition

On the basis of the above experimental observations, the following two schemes in which  $O_2$  participates can be suggested to explain the deposition of  $B_2O_3$  on SiO<sub>2</sub> surface in the process of vapor decomposition:

Scheme 1:

$$B(OEt)_3 \xrightarrow{O_2} B_2O_3 \xrightarrow{SiO_2} B_2O_3/SiO_2$$

Scheme 2:

$$B(OEt)_3 \xrightarrow{SiO_2} \xrightarrow{O_2} B_2O_3/SiO_2$$

According to Scheme 1,  $B_2O_3$  is formed by the combustion of  $B(OEt)_3$  in the gas phase to be directly deposited on the  $SiO_2$ surface. In Scheme 2, first  $B(OEt)_3$  reacts with the hydroxyl groups of  $SiO_2$  surface forming Si—O—B bonds, and then the residual ethoxy groups on boron are oxidized to form surface B—OH groups;  $B_2O_3$  can be deposited on SiO<sub>2</sub> surface through repetition of these surface reactions. If the vapor decomposition process proceeds via Scheme 1, a certain  $B_2O_3$  deposition should be observed also on the internal wall of the reactor. The deposition of  $B_2O_3$ , however, was never observed on the reactor wall around the SiO<sub>2</sub> bed, and in contrast with the case of vapor decomposition using H<sub>2</sub>O, no preferential B<sub>2</sub>O<sub>3</sub> deposition occurred on the upper side of the  $SiO_2$  bed. Moreover, it was confirmed that only a trace amount of  $B_2O_3$  (0.8 wt%) was deposited by the vapor decomposition of B(OEt)<sub>3</sub> in a stream of  $N_2$ , but a certain amount of  $B_2O_3$  (4.0 wt%) could be introduced through repetition (18 times) of a pulse procedure which involved the vapor decomposition of  $B(OEt)_3$  in a stream of  $N_2$  followed by the combustion with air. These results suggest that the vapor decomposition with  $O_2$  in the present study proceeds substantially via Scheme 2.

When the vapor decomposition was performed at 400°C, more  $B_2O_3$  was deposited on the upper side than on the lower side of the SiO<sub>2</sub> bed. This undesirable phenomenon was probably due to an increase in the rate of  $B_2O_3$  deposition at higher temperature. In addition, the SiO<sub>2</sub> particles were adhered each other with  $B_2O_3$  melt at 400°C. At higher temperatures, the reaction via Scheme 1 may be predominant.

In the vapor decomposition procedure using a fixed-bed apparatus (Fig. 1), a gradient of  $B(OEt)_3$  concentration through  $SiO_2$ bed may cause a little difference in the rate of  $B_2O_3$  deposition between upper and lower sides of the  $SiO_2$  bed. In order to assure more uniform vapor decomposition of  $B_2O_3$  onto  $SiO_2$  throughout the support bed, it seems convenient to use a rotary reactor or a fluidized-bed reactor. The study on the vapor decomposition using a rotary reactor is now under way.

## Catalytic Feature of Vapor Decomposition B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub>

It is obvious that vapor decomposition  $B_2O_3/SiO_2$  is more active and selective than impregnation  $B_2O_3/SiO_2$  (Fig. 5). The most active  $B_2O_3/SiO_2$  catalyst for the Beckmann rearrangement was obtained through vapor decomposition performed at 350°C for 3 h at a B(OEt)<sub>3</sub> feed rate of 3.5 mmol/h. The lactam selectivity, however, was dropped when vapor decomposition was carried out either at 400°C for 3 h (Fig. 3) or at 350°C for more than 3 h (Fig. 4). The selectivity drop may be due to the change in acid property of catalyst through high-temperature or long-time operation of vapor decomposition which causes melting of a part of  $B_2O_3$  crystallites. In fact, at 400°C, the SiO<sub>2</sub> particles were adhered to each other with glassy  $B_2O_3$ . In this context, it was confirmed experimentally that B<sub>2</sub>O<sub>3</sub> alone without support was quite inactive for the rearrangement reaction (oxime conversion, 4.0%; lactam selectivity, 26.4 mol% at  $300^{\circ}$ C), and that after the reaction B<sub>2</sub>O<sub>3</sub> particles changed into a glassy melt with a very small surface area. This fact suggests that melting of  $B_2O_3$  may be also responsible for the decreases both in activity and in selectivity.

The change in BET surface area with  $B_2O_3$ content (Fig. 7) as well as the comparative SEM images of  $B_2O_3/SiO_2$  (Fig. 8) clearly suggest that the SiO<sub>2</sub> surface is uniformly covered with B<sub>2</sub>O<sub>3</sub> by means of vapor decomposition. On the other hand, the present impregnation method involves a step of calcination of the supported  $H_3BO_3$ , so that  $H_3BO_3$  is prone to aggregate into large B<sub>2</sub>O<sub>3</sub> particles in the course of dehydration leaving the SiO<sub>2</sub> surface free from the accumulation of  $B_2O_3$ . Since SiO<sub>2</sub> itself is inactive for the rearrangement reaction and furthermore the exposure of SiO<sub>2</sub> surface is not preferable to enhancement of the lactam selectivity (Fig. 5), it is necessary for obtaining an efficient B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> catalyst to cover the SiO<sub>2</sub> surface with B<sub>2</sub>O<sub>3</sub> uniformly and completely as exemplified by a vapor decomposition catalyst having a  $B_2O_3$  content of 34 wt%. According to our preliminary study on the vapor decomposition of B(OEt)<sub>3</sub> onto  $\gamma$ -alumina (4), a  $B_2O_3$  content between 20 and 25 wt% was enough to cover the alumina surface to give the most active rearrangement catalyst, because the surface area of the alumina was smaller (160 m<sup>2</sup>/g) than that of the SiO<sub>2</sub> used in the present study (281 m<sup>2</sup>/g).

The result of the measurement of DHA (Fig. 11) indicates that the most active vapor decomposition  $B_2O_3/SiO_2$  possesses much more effective acid sites whose DHA values are at least 80 kJ/mol, compared with the most active impregnation  $B_2O_3/$  $SiO_2$ . Since the maximum DHA values are almost the same for both catalysts, the average acid strength of the vapor decomposition catalyst must be greater than that of the impregnation catalyst. This reasoning is in good harmony with a result obtained in the TPD measurement that the pyridine desorption peaks observed with vapor decomposition catalysts shifted to the higher temperature side compared with those observed with impregnation catalysts (Fig. 10).

Reportedly, a DHA value of 76 kJ/mol corresponds to a p $K_a$  value of -5.6 (10). According to our qualitative measurement of acid strength by use of the Hammett indicators, both vapor decomposition and impregnation B<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> could change Benzalacetophenone ( $pK_a = -5.6$ ) into its acidic color, but SiO<sub>2</sub> could change only Dimethyl Yellow ( $pK_a = +3.3$ ). Since SiO<sub>2</sub> support itself (DHA < 80 kJ/mol) is inactive for the Beckmann rearrangement, it can be deduced that the acid sites of  $B_2O_3/SiO_2$ whose acid strengths are less than -5.6 in terms of  $H_0$  should be responsible for catalyzing the rearrangement reaction. In addition, the acid strength of vapor decomposition  $B_2O_3/SiO_2$  was found reasonably uniform, judging from the flatness of DHA curve.

In conclusion, higher catalytic activity

and selectivity of vapor decomposition  $B_2O_3/SiO_2$  for the Beckmann rearrangement in comparison with impregnation  $B_2O_3/SiO_2$  should be attributed to a larger amount of effective acid sites in addition to more uniform acid strength. Such favorable acid property was obtained through uniform deposition of  $B_2O_3$  by means of vapor decomposition.

#### ACKNOWLEDGMENTS

The authors thank JGC Corporation for measuring the differential heat of adsorption of ammonia and the pore size distribution, and they also thank Fuji Davison Chemical Ltd. for supplying  $SiO_2$  supports. This work was supported in part by the Grant-in-Aid for Scientific Research (No. 60550584) from the Ministry of Education, Science and Culture, Japan.

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